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SUS QUALITY ASSESSMENT, SQUARE DEAL

Marvin S. Weinstein, et al

Underwater Systems, Incorporated

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Kingsport during the SQUARE D	EAL Exercise	for SUS signals were pro-
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tion depths of those shots know	own to a high	degree of confidence
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FINAL REPORT

SUS QUALITY ASSESSMENT SQUARE DEAL

February 7, 1975

Prepared by:

M. S. Weinstein L. A. Mole

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SUS QUALITY ASSESSMENT SQUARE DEAL

Summary

The detonation pressure time curves recorded aboard the USNS Kingsport during the SQUARE DEAL Exercise for SUS signals were processed to acquire quality assurance statistics. Bubble pulse periods were determined for each detonation from which an equivalent depth was derived. Because the SUS signals were received by a hull mounted transducer with poor characteristics, many of the shots recorded exhibit distortion and ringing. This lowers the quality of the data and reduces the confidence that can be attached to the shots processed. For this reason, it is recommended that only those shots known to a high degree of confidence to be within ±10% of the scheduled detonation depth of 300 ft (bubble pulse period: 39,0 to 45.4 msec) be deemed acceptable for further processing. Those shots known accurately to be outside of this range should be rejected. For the vi shots which exhibit distortion and ringing, signals received at the acoustic stations should be processed by narrow band analysis to determine their bubble pulse periods and rejected if they fall outside of the specified limits, when the measured propagation loss is suspect.

Introduction

During the SQUARE DEAL Exercise, a series of
SUS shots were deployed by the USNS Kingsport for the
purpose of measuring acoustic propagation loss. Quality
assurance procedures were instituted to ensure that the
data obtained would not be affected by variations in
source level or detonation depth. Magnetic tape recordings
of the SUS pressure signals were obtained from the USNS
Kingsport. In a manner analogous to an earlier program,
Ref. (1), these tapes were processed to determine the
bubble pulse period from each of the SUS shots used for
the propagation loss studies. From the bubble pulse
period of the source, deviations in shot depth and band
levels can be determined. The processing technique,
results, and recommendations are presented forthwith.

Basic Data and Instrumentation

The shock wave and bubble pulse signatures emitted from the SUS charges were monitored by mounting a voice powered microphone to the hull of the Kingsport with a C-clamp. The ship's hull was used to couple the SUS pressure signals from the water to the microphone. These signals were subsequently recorded in the FM mode on magnetic tape. A l kHz tone and time code was recorded

in the FM mode and voice annotations were recorded in the direct mode. Approximately 1019 Mk 82 shots were dropped and detonated at 300 feet. A listing of results is given in Table (1).

Although the ship's hull resonants, this did not appreciably affect the signature appearing at the output of the microphone as long as the microphone was securely clamped to the hull. However, the vibrations did result in loosening the C-clamp that was holding the microphone, causing spurious signals that appear as "ringing" at the microphone output. This ringing reduces the confidence to which the shock wave and bubble pulse can be correctly identified. This signal distortion necessitated a significant change in the processing procedures employed in Ref. (1) in order to analyze the shots. Severe filtering permitted the identification of these signal components, with a considerable loss of resolution.

From the above description of the instrumentation for monitoring the shock wave and bubble pulse, it is obvious that the classic shock wave and bubble pulse signature as emitted from a SUS detonation will not be observed at the microphone output. In order to obtain the classic signature, it is necessary to judiciously place a hydrophone or shock wave gauge in the water.

TABLE 1
Tabulation of SUS Statistics
SUS Type MK 82, 1.8 lb

Experimental Area	1C - 1A	2D - 2BD	
Date	9-10 Aug. 1973	16 Aug. 1973	
Number Dropped	577	442	
Number Processed	552	415	
Number Not Recorded	2	7	
Dud	17	16	
Wrong Explosive Charge Depth Setting	6	4	

Data Processing System

A block diagram of the data processing system is shown in Figure (1). The data from the tape recorder is preprocessed before being digitized for processing.

The computer provides four functions: (1) system controller, (2) data interrogation, (3) determination of bubble pulse period, and (4) display controller. The operator's chief function is to serve as an on-line quality assurance monitor. To assist him in this role, the shot is displayed together with the computer determined bubble pulse period on an oscilloscope for immediate observation, and at the operator's option, a hard copy can be made for further study. Shot identification and bubble pulse periods are presented on the TTY printer.

This set of shots required more processing than the series done previously, Ref. (1). The data channel from the recorder is amplified to convert a nominal 1 volt rms signal from the recorder to a 10 volt peak signal for input to the 13 bit analog to digital converter. The channel is sampled at a nominal 8 kHz derived from the 1 kHz tone. This 1 kHz signal is utilized to furnish a reference frequency to remove tape recorder speed errors. This signal is filtered, limited, and multiplied by 8 in a phase locked loop. The synthesized frequency is then used as the sampling pulse for the A-D converter. The absolute levels of one of the shots processed in this way is shown in Pigure (2).

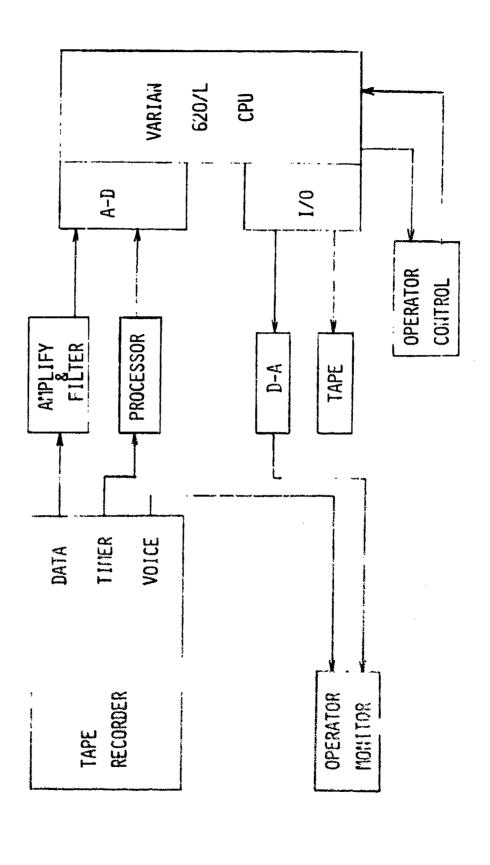


FIGURE (1). BLOCK DIAGRAM OF BUBBLE PROCESSING SYSTEM

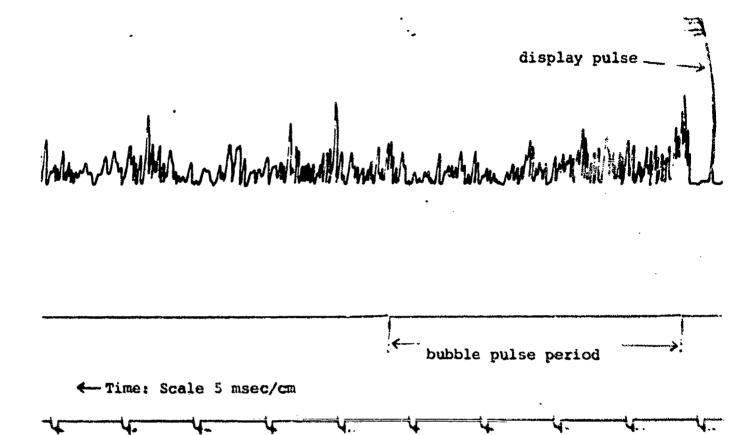


Figure (2). Typical unprocessed SUS signal display at 1/5 normal time scale (shot #328 1C to 1A). Pull wave rectification applied

As is apparent, while it is possible to ascertain the shock-wave onset the bubble pulse signal cannot be identified. Consequently, several different methods were tried to enhance the signal to noise ratio and to make the bubble pulse period determination easier. Filtering the signal to obtain a clearer pattern was attempted; including band pass, low pass, and high pass techniques. The method finally chosen was to amplify the signal voltage, input it through a 1/3 octave 800 Hz filter, square this output, and then sample the result. The shot shown in Figure (2) is shown again in Figure (3) after this processing has been done. The signal to noise ratio has been enhanced and the shockwave and bubble pulse are discernible.

After a shot is detected and processed, the computer through a D-A converter to an oscilloscope, repetitively outputs, as in Figure (3), the digitized shot together with two pulses. One pulse marks the shockwave maximum level and the other the bubble pulse maximum. This display is used by the operator to evaluate the quality of the determination. The option also exists to output the scope display on the chart recorder at a scale factor of 1.0 msec/cm for further study.

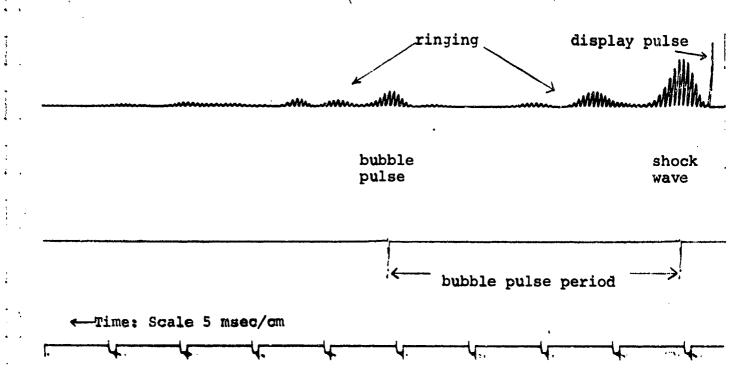


Figure (3). Typical processed SUS signal display at 1/15 normal time scale (shot #328 1C to 1A)

Using the measured bubble pulse period and assuming an explosive charge of 1.8 lbs of TNT; the detonation depth is derived from the following formula, Ref. (2):

$$T = \frac{4.36 \text{ w}^{1/3}}{(\text{d}+33)^{5/6}}$$

where,

T = bubble pulse period

W = charge weight

d = detonation depth

The curve for T as a function of d was fitted with a polynomial, and this was used to derive the detonation depth from the bubble pulse period.

Computer Operation

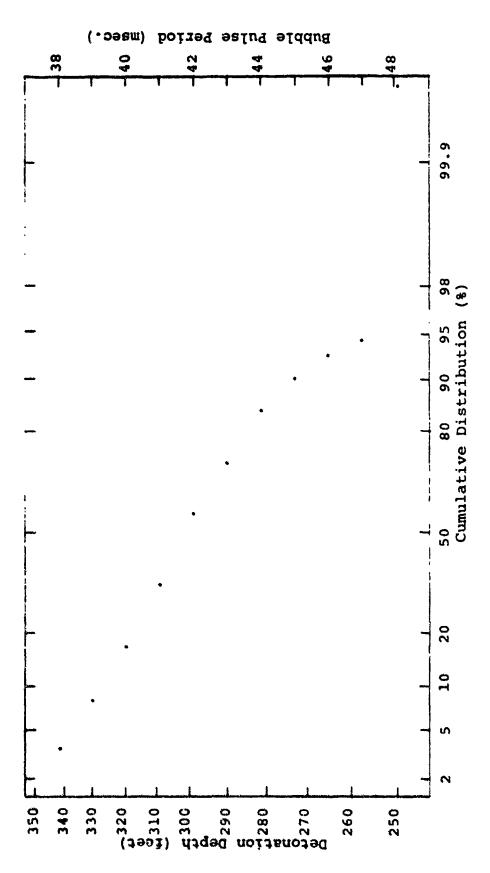
The design of the system minimizes the recurrent menial tasks that the operator must perform so that he can concentrate on evaluating each bubble pulse determination. During a run, the computer monitors the data channel until the onset of a shockwave exceeds a preset level. When this happens, the block of digitized data which follows is stored. Then the peaks of the shockwave and the bubble pulse are determined by recurrent looks at the stored data with successively lower comparative levels. The use of this analysis procedure on the shockwave is necessitated because of the type of preprocessing done

on the data. The search for the bubble pulse peak is restricted to a time span from 37.0 to 48.0 msec from the shockwave peak. Restricting the bubble pulse search to these limits is necessary to handle the ringing problem introduced by the method of transducer mounting. If a suitable bubble pulse peak is not found, an alarm is sounded to alert the operator of a possible mis-determination. The determination is then displayed.

Processing Results

A total of 1019 SUS shots were launched by the Kingsport on the two runs, from 1C to 1A (9-10 August 1973) and 2D to 2 BD (16 August 1973). Of that number, 967 shots were processed and the remaining 5% consist of Duds, and unprocessable detonations. Table (1) summarizes this information. The cumulative distributions as a function of the bubble pulse period and shot depth for the two runs are presented in Figures (4) and (5). The most likely bubble pulse period in mach case is very close to the expected nominal value. i.e. a value of 41.9 msec.

Although the agreement between the experimentally determined bubble pulse periods and the theoretical value is good, the signal distortion problems encountered result in a low confidence level. To illustrate this point, three consecutive shots have been selected from the 9-10 August 1973 1C to 1A run of the Kingsport. These three figures,



Cumulative Distribution of Bubble Pulse Period and Derived Shot Depth for Run IC-1A. Figure (4).

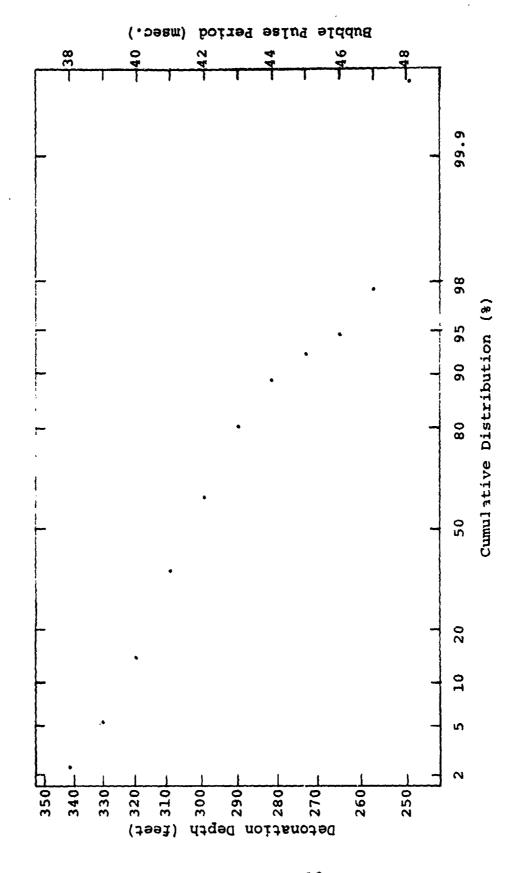


Figure (5). Cumulative Distribution of Bubble Pulse Period and Derived Shot Depth or Run 2D-2BD.

(6) through (8), show the D-A output display from the computer of the amplified, filtered, and voltage squared bomb shot. The gain of shots \$328 and \$330 are the same, while that of \$329 is +10 db higher. These three figures indicate the ringing problem clearly. As the C-clamp loosened, the pattern first showed slight ringing (\$328), then a very bad pattern (\$329), and finally a good pattern (\$330) when retightened. This effort complicated the processing since signal strength varied from five to fifteen db between shots. Since a detection level of 2.5 volts was used and the A-D input voltage was limited to 10 volts, the tape recorder had to be frequently backed up and gains changed in order to "capture" the shot.

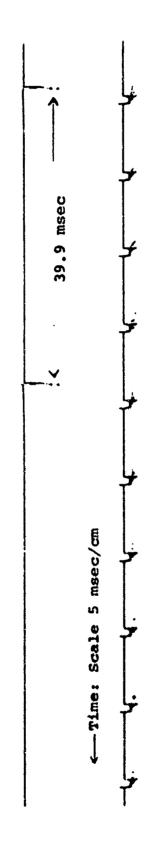
Although the signal distortion made processing difficult but not impossible, the main effect of the ringing, as in shot #328, was to obscure the presence of the bubble pulse. For this reason, the scan for the bubble pulse was limited to between 37 and 48 msec. However, for some shots, it was impossible not only for the computer but also for a scientist to pick the correct peak out of several appearing in this range. A chart recording was made for each of these shots to facilitate any additional analysis.

40.5 msec - Time: Scale 5 msec/cm

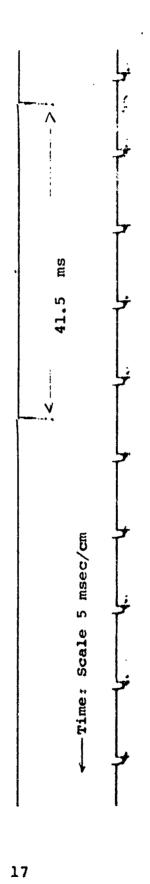
Figure (6). Shot #328, 9 August 1974, 1C - 1A USNS Kingsport

15

T



Shot #329, 9 August 1973, 1C - 1A, USNS Kingsport +10 db gain relative to shots #328 and #330 Figure (7).



ı

Figure (8). Shot #330, 9 August 1973, 1C - 1A USNS Kingsport

Those shots known to a high degree of confidence to be outside of the 270 to 300 ft range, which are to be rejected, are listed in Table (2). For those shots listed in Table (3), for which confidence in determining the bubble pulse period is low, we recommend that the narrow band spectra of a received signal, with good signal to noise ratio, be examined. The bubble pulse period can be determined in that fashion. If it falls outside the specified region, the shot should be rejected. A complete listing of all shots processed is given in Tables (5) and (6).

Data Selection and Source Level Corrections

Because of the poor resolution resulting from the severe filtering necessary to identify the bubble pulse, the accuracy of the measurements is not sufficient to warrant the application of source level corrections.

However, if it is desired to do this, the correction functions are given in Table (4). This table is a composite of calculations based on the Weston and Gaspin and Shuler formulations, as in Ref. (1), except that new computations of the Gaspin and Shuler formulation have been provided to us by NSWC in private communications.

It is recommended that only shots within 110% of the scheduled detonation depth (bubble pulse period, 39.0 to

TABLE 2
SUS Shots Which Should Not Be Used
Detonation is Outside of ±10% of 300 ft

Run	1C -	1A			9,10	August	1973		
25	38	51	59	85	87	106	109	111	126
127	129	130	151	169	174	180	193	195	198
218	242	243	246	256	259	263	266	284	305
307	309	323	324	326	334	343	344	404	406
407	435	436	437	455	460	488	491	496	511
520	533	545	549	557	570	575	596	602	610
Run	2D -	2BD			16 Au	igust 19	73		
71	72	73	77	137	143	150	155	173	177
186	191	201	205	291	313	338	401	407	412

TABLE 3
SUS Shots with Low Confidence

Rur	1C -	1A		9,	,10 Aug	just 1	973		
14	17	18	33	34	50	53	71	72	74
90	86	104	121	125	135	140	145	154	161
163	164	181	187	209	213	216	221	225	230
245	247	253	254	255	257	258	264	268	269
321	329	336	338	352	403	409	411	412	428
432	441	447	448	454	461	464	474	480	487
495	497	508	516	541	572	597	609		
Rui	2D -	2BD		16	5 Augus	st 197	3		
5	15	18	21	31	49	50	57	59	92
97	101	108	116	124	129	132	135	138	149
159	165	197	215	222	246	247	248	250	254
260	264	275	278	279	295	304	314	316	318
349	369	376	379	380	381	382	400	416	424
429	430	438							

TABLE 4

Spectral corrections for square 1/3 octave bands. Corrections in db to be added to the nominal levels for 1.8 lb detonated at 300 feet.

Detonation		Center	Preque	ncy	
Depth (ft)	25	50	100	160	250
270	+0.5	0.0	0.0	-0.5	+1.0
280	+0.5	0.0	0	-1.0	+1.0
290	0.0.	0.0	0.0	-0.5	+0.5
300	0.0	0.0	0.0	0.0	0.0
310	0.0	0.0	0.0	0.0	+0.5
320	-0.5	0.0	0.0	0.0	+1.0
330	-1.0	0.0	0.0	0.0	+1.0

45.4 msec) be processed provided that they were not among those exhibiting distortion. As can be seen from Table (4) the variation in source level, resulting from not applying correction, will then be limited to about to one decibel.

Quality Control

period have two origins, (1) the basic data, and (2) the measurement of the bubble pulse period. Any tape speed variations on record and playback will affect the measured time. In the present processing scheme, the 1 kHz tone was used for controlling the sampling rate and hence the relative change in tape speed variations are removed.

As in Ref. (1), the phase lock loop error voltage was checked periodically to verify proper synchronization.

The bubble pulse period is defined as the time bounded by the onset of the shockwave from the explosion and the bubble pulse maximum. Because of the filtering that was necessary to process the signals, the maximum of the shockwave was chosen as the lower bound of the bubble pulse period. A check was made throughout the processing of the decisions made by the computer in chosing the maximum levels. In all cases the computer picked the largest peak within the scanned time frame. The bubble pulse periods determined with a high degree

of confidence have a repeatability to within 0.5 msec, however, the absolute accuracy is probably not as good. Those shots processed which contain ringing have several distinct peaks or several smeared into one. The proper bubble pulse can not be ascertained in these cases, as have been previously noted, and repeatability is poor.

TABLE 5

SUS SHOT STATISTICS FOR SQUARE DEAL

	for usus	King Sport	DURING AU	WRING AUGUST, 1973		
	skot 0	APPROXINATE DETONATION TIME (ZULU)	Bubble Milse Period (MSEC)	CALCULATED SHOT DEPTH (FT)	Comment Code	
	4	09055820	43.0	890	_	
		09055420	41.8	301	-	
	3	09055620	41.9	301	_	
	4	09055820	43.6	284	-	
	5	09060020	40.9	310	_	
	6	09060280	43.0	290	•	
	7	09060420	3978	321		
	8	09060620	44.9		•	
	9	09060820	40.8	273	•	
	•	09061080		311	•	
	10		48.3	297	•	
	11	09061920	42.8	298	•	
	12	09061480	43.8	283	•	
	13	_ 09061620	40.6	318	•	
	14	09061820	47.9	251		
	15	09065080	,		1	
	16	09068550	41.0	309	•	
	17	09068480	47.6	253	, 👁	
	18	09062620	47.9	291	•	
	19	09068820	••		1	
	20	09063020	42.1	298	-	
	81	09063220	40.6	312	•	
	22	09063420	44.0	26 t	ھ ۔	
12	23	09063620	43.3	288	•	
	84	09063820	38.9	331	•	
11	25	09064020	45.6	267	-	
	28	09064220	41.8	301	•	
10	27	09064480	41.0	309	•	
	88	09064680	42.6	293	-	
ý	29	09064820	41.6	308	_	
·	30	09065080	43.5	285	_	
8	31	09065220	41.0	309	_	
U	38	09065480	43.0	290	~	
,	33	09065680	43.8	290 263	-	
,	34	09065820	47.6	253	- .	
	35	69 070080			•	
٠		09070220	44.8	275	₩.	
	36		40.8	311	-	
5	37	09070420	43.0	290	⇒	
	36	09010620	37.5	347	•	
4	39	09070820	41-0	309	•	
	40	0907 1020	40.a	315	44	

	41	09071820	39.5	384	•
	48	09071480	39.5	324	•
	43	09071620	43.0	290	ä
	44	09071820	41.3	306	
	48	09072020	43.5	285	•
	46	09672820	48:1	298	
	47	09072480	41.0	309	<u>.</u>
	48	09072620	41.4	305	
	49	09078830	38.8	338	_
		09073020	3774	349	ä
	60	*	47.5	254	
	51	09073889 		303	 6
	52	_09 6 7 <i>9</i> 480	41.5		
	83	09073620	49.5	253	
	54	05073820	39.4	326	•
_ ,	55	09074020	39.4	383	•
	56	09074220	39.3	387	•
	_57	09074420	43.3	246	•
	58	09074620	45.3	270	æi
	59	09074820	47.4	255	•
•	60	0907 5020	41.5	303	=
	61	_09075220	43.1	289	•
	68	09075420	42.1	2 98	•
	63	09075420	40.5	314	•
	64	09075820	43.3	888	*
	65	09080080	39.5	384	•
	66	09080220	29.8	311	ä
	67	09080420	44.9	873	<u>.</u>
	68	09060620	39.6	383	•
	69	_09080820	44.9	273	ė
	70	09081020	42.4	295	•
	71	09081880	39.9	380	•
	72	09061420	47.8	252	•
	73	09081680	38.1	339	• .
	74	09061620	38.9	331	•
	75	09082020	43.9	262	•
	76	09082220	41.0	309	=
	77	09082420	41.5	308	
	78	09088650	48.3	897	68
	79	09098880	68.8	898	<u>.</u>
	80	09083020	37 . 9	362	•
	81	09083220	40.9	310	÷
	82	09033420	39.4	386	•
	63	09053680	41.6	308	•
	84	09083620	44.0	881	•
	88	09084020	47.8	252	•
- • •	26	09064820	42.1	298	⇔
	57	09054480	3766	347	0
	60	09064620	4104	305	•
	86	09084580	. 48-4		<u>.</u>
	90	09055020	40.4	315	-
	98	09083280	41.3	304	•
	92	09085420	45.1	27 1	•
			• •		

	93	09085620	43.3	288	•
	94	09088880	43.1	247	=
	95	09090020	45.0	27 #	=
	93	09090220	41.9	301	•
	97	09090480	41.1	307	•
	98	09090680	41.8	301	16
	99	09090880	•	••	3
	100	09091080	40.9	310	•
	101	09091220	41.9	301	•
	102	09091480	39.5	324	•
	103	09091620	41.1	307	<u>.</u>
	104	09091820	42.0	299	÷
	105	09092020	43.3	285	•
	106	09092220	37.0	384	_
	167	09 092420	48.1	295	ai
	108	09092620	48.4	295	•
	109	09092620	38.8	332	•
	110	89093020	40.9	310	
	111	09093880	38.3	336	
	118	09093480	39.6	321	^ ;;
	113	09093420	41.8	307	•
	114	09093680	41.9	301	ė
	115	09094020	43.8	263	-
	116	69094220	41.0	309	::
	117	09094420	40.0	319	•
	118	09094680	41.8	301	
	119	09094620	42.8	292	
	180	09096020	41.4	305	
	181	09095220	40.3	316	•
	128	09098480	39.9	380	•
	123	09095620	41.9	301	-
	184	09095820	43.9	252	
	125	09100080	43.1	259	•
	186	09100220	45,6	267	•
	127	09100420	46.8	264	•
	1 28	09100480	39.8	381	•
	189	09100820	47.0	257	-
	136	09101020	38.0	336	•
	131	09101820	40.6	341	•
	132	09101420	44.1	279	•
	133	09101620	40.0	319	
	124	09101820	41.9	301	
	135	08080190	47.0	257	•
	136	04145550	41.4	305	•
	. 3·	09102420	4163	304	•
•	138	09102690	44.4	278	•
	139	09102890	4075	314	•
•	140	09103020	43.3	288	*
	141	09103220	41.0	309	•
	148	09103420	41:3	306	=
	143	09103480	40.8	311	•
	144	09880190	43.0	890	•

	145	09104020	47.0	257	•
	146	09104880	42.8	292	•
	147	09104420	40.9	310	•
	148	09104620	41.4	305	•
	149	09104820	*	.,	1
	150	09105080	43-4	256	•
	151	09108220	45.5	268	•
	158	09105420	40.4	316	•
	163	09108620	48.0	299	•
	184	09105520	40.9	310	ė
	155	09119020	41.8	301	
	156	09119220	48.6	293	<u>.</u>
	187	09110420	44.4	276	ý
· · · · · · · · · · · · · · · · · · ·	156	09110680	40.8	311	•
	159	09110880	41.6	308	•
	160	09111020	40.9	310	•
	161	09111820	41.9	301	<u> </u>
	162	09111420	39.1	389	.
	163	09111680	45.5	268	•
	164	09111890	4668	259	•
	168	09112020	43.6	864	ė
	166	09116820	48.4	896	
	167	09112420	40.9	310	
	168	09112620	41.6	300	
	169	09112820	38.3	336	
	170	09113020	43.9	262	•
	871	09113820	43.3	288	•
	172	09113480			1
	173	09113620	41.4	305	
	174	09113620	45-6	257	ė
	175	09114020	41.4	305	<u>.</u>
	176	09114880	44.4	278	· · · · · · · · · · · · · · · · · · ·
	177	09114420	48.6	293	-
	178	G9114680	42.0	299	-
	179	09114380	4101	307	- -
	180	09115080	37:4	349	<u>.</u>
	181	09115820	37.1		<u>-</u>
	188	09113420	39.4	359 386	
	163	09115480	41.6	301	₩
	184	09118820	41.1	307	-
	169	09180080	38.9	331	⊕
	166	09120920	48.1	29 2	-
	187	09180480	43.1	\$89	<u> </u>
	166	09190690	39.4	326	
	169	09120520	42.9	290 280	_
	190	09121020	40.6	215	_
	191	09181880	45.1	87 i	±5•
	198	09181480	41.5	303	- .
	193	09151650	37.9	343	_
	194	09131820	41.0	309	
	198	09188080	37.4	349	444
	196	09192920	41.4	34¥ 36 <u>9</u>	<u>.</u>
		v	42 E 51 C 5	477.034	

	197	09138430	(\2 - 5	294	•
	198	09122680	46.5	261	•
	199	04122820	43.0	290	•
	800	09123020	4875	294	ä
	201	09183820	42.0	28.9	•
	206	09183480	A1.5	303	~
	203	09123620	40.0	319	•
	204	09123820	40.6	312	•
	205	09124020	39.3	387	÷
	206	09124220	43.9	865	
	207	09124420	41.4	305	.
	205	09124620	40.6	316	
	209	09124820	42.0	299	
	810	09125020	40.3	316	•
	811	09125220	41.8	301	•
	818	09125480	7		1
	213	09125420	42.9	290	
	214	09125820	43.6	284	.
	215	09130020	43.6	283	_
	216	09130220	40.9	310	-
	817	09130420	40.5	310	•
	218	09130620	47.6	080	1
	519	09130880	41.4	252	•
	580	09131080	40.9	30 5	•
	85 ! 224	09131880		310	•
	929	09131426	43.6 42.9	254	•
	823	09131620	40:4	290	•
	224	09131820	4173	315	•
	225	09132020		306	•
	886	09138550	49.1	884	•
			41.8	301	
	<u>927</u> 928	<u>09138480</u>	3915	384	. ,. 🖜
	22 9	09138680	41.4	305	•
		09138620	41.4	305	•
	830	09133080	41.8	254	•
	231 232	69133820	41.0	30 9	•
		09133480	42.9	290	•
	833	09133620 09133620	48.3	897	··· · · · · · · · · · · · · · · · · ·
	234		43.6	284	•
	235	09134020	48.4	899	•
	236 237	09 134220 09 134420	41.6	308	•
	238 238	09134620	40.5	314	~
	239	09134880	44.6	275	•
		natural control of the first term and the same of th	43.3	286	• .
	240	09135020	41.0	309	•
-	241	02286160	48.3	£97	•
	248	09135420	47.5	264	ee .
	843	09139680	37.4	349	• .
	244	09135620	41.5	303	
	245	<u> </u>	37.9	343	, •
	244	69140820	38.3	225	•
	847	09140420	47.6	963	•
	245	09140620	43.0	800	•

	444	0011000	A 60 A	224	
	849	09140880	43.4	266	•
	250	09141020	41.6	391	•
	261	09141220	4171	307	•
	268	0914148 0	41:1	367	43
	253	08141620	47.6	853	٠
	254	091416 <u>8</u> 0	39.0	329	•
	255	09142020	43.4	286	•
	255	09148880	47:1	856	•
	257	0914242 0	45.1	871	•
	252	09142468	47.0	257	
	859	09148880	4506	267	•
	246	09143030	40.9	310	•
	861	69143880	4411	279	•
	258	69143880			1
	269	09143480	37.0	354	ì
	244	09143820	48.5	294	
	865	09144080	41.1	307	
	846	09144220	47:4	255	
	267	69144480	49.9	290	-
	268	09 44680	40.1		
	269	09144620		316	•
	270	09145020	3974	386	•
	271	09145280	90 6	90 4	8
-			39.5	384	•
	87 8 000	09145480	40.1	318	-
	673	09145620	4165	303	=
	274	09 (45520	48:1	298	•
	975	09180650			ï
	276	09150280	39.3	327	•
	277	09 I 504 & O	4370	863	•
	27 B	09 150620	39.5	384	
	279	69150820	44.0	25)	•
	230	09181020	41.1	307	~
	25]	09151820	40.5	314	<u>=</u>
	252	09151420	•		1
	283	09181620	40.5	314	ê
	254	09131820	38.8	338	-
	255	09148080	41.4	308	ė
	236	09162880			1
	267	09152420	42.5	202	à
••	255	091 5 2620	46.8	275	•
	239	091 \$2080	41.9	301	•
	290	09163020	40.3	316	æ
	291	691 83880	40.6	381	•
	068	09153490	43.0	890	•
	293	69183620	48.0	899	
	230	09153880	48.5	894	÷
	293	09154080	48.0	899	
	276	09154820	49.4	208	• .
	897	09154490	44.6	£7 6	•
	898	09184680	39.9	380	
	299	09154520	4374	286	•
	300	07165020	48.5	894	•
			74 T W		_

	301	09155820	44.1	276	•
	302	09188420	39.6	383	
	305	69155420	39.3	387	=
	304	09158890	81.6	302	 •
	305	09160020	4576	867	.
	306	09140220	48.4	895	•
	367	09140420	38.9	331	•
	308	09150620	41.8	303	-
	309	09140820	38.5	338	
	310	09141020	48.4	295	ø.
	311	09161920	39-1	389	•
•	318	09161420	41.1	307	Ġ
	313	0916140	44.8	275	
	314	09161529	39.6	323	
	315	09162020	41.5	303	=
	316	09162880	42.0	299	-
	319	09162486	42.9	290	÷
	316	09162620	41.1	309	•
	319	09886190	41.4	305	
	320	09143020	40.6	311	
	321	09163820	47.5	834	•
	392	09163480	41.3	306	
	383	09163620	47:0	257	œ.
	384	09163880	37 6	346	•
	385	09164020	41.3	306	
	326	09164220	47:4	255	-
	327	09164420	39:1	389	•
•	328	09164620	40.0	319	
	389	09164520	43.6	284	
	330	09165020	40.4	305	
	331	09165920	41.6	301	_
	332	09165490	Alil	307	· · · · · ·
	333	09148620	41.6	302	<u></u>
	334	09168890	47.8	258	<u>.</u>
	335	09170020	41.1	307	- -
	335	09170220	42.8	292	
	337	09170420	• • • •		1
	338	09170680	42.4	295	~~ <u>}</u>
	339	09170820	41.9	301	•
•	340	09171020	39.3	327	_
	341	09171220	40.4	318	
	349	09171420		• • • • • • • • • • • • • • • • • • • •	1
	343	09171820	38.9	331	
	244	09171880	45.4	269	G
	345	09172020	41.9	301	=
	346	09172220	42.6	293	•
	347	09178480	42.0	860	-
	348	09178680	41.0	309	i i
	349	09172920	41,6	302	•
	350	09173020	41.9	301	•
	381	09173220	40.4	315	
	350	09173480	AlaA	305	2

	353	09173620	42.5	894	•
	354	09173820	44.9	273	4 3
	355	09 17 4020	42.9	290	.
	354	69 174220	41:5	303	•
	357	09174420	39.9	380	iii
	358	09174620	39:8	321	\
	359	09174520	39.3	387	\bullet
	400	09175020	40.6	318	•
	401	09175820	4111	307	ė
	402	09175426	48.4	29 5	œ
	403	09175620	41:5	303	
	454	09178680	37:0	354	;;
	405	0 9 1 5 0 0 2 0	39%	323	•
	406	04 180350	35.9	331	•
	407	09180420	38:6	334	•
	405	C418C420	41:5	303	÷
	409	6 7 1 5 0 6 2 0	4476	275	ė
	410	09181020	48.4	898	
	411	09181920	49.6	312	43
	412	09181420	37.3	360	
	413	C2318100	**	•	1
	414	09181820	39.3	367	ë
	415	67 182020	40%6	318	4
	416	02288140	41.6	301	÷
	417	69188480	48.5	294	
	415	09158680	40.8	311	<u></u>
	419	00162820	4076	312	÷
	420	09183020	42.1	898	
	421	09153990	48.6	293	· · ·
	422	09163420	42.5	894	:
	423	09163620	41.4	305	ie.
	424	09183880	43.1	239	
	425	09184020	41.0	309	•
•	486	00184280	•		2
	487	69184480	39.6	321	6
	483	09184620	43.4	686	4
	489	09164620	42.3	297	::
***************************************	430	09185020	43.6	884	
	438	69165220	46.0	265	•
	634	69 188420	•••	- F	
	435	00165620	47.5	252	Ĩ
•	636	09185820	38.1	359	•
	437	02198020	38.5	236	•
	435	0#196980	39.0	288	
	439	69190420	39:3	397	•
	640	09190620	49.1	808	•
	401	09190820	36.8	334	•
	442	02016160	43.0	890	•
	463	09191690	•••		1
	986	09191420	40.6	311	•
,	445	04141650	4973	686	ä
,	446	02219160	48.4	312	-
		i i			

	447	09198380	39.4	386	•
	345	09199880	37:0	343	•
	449	09192420	40.4	315	¥
•	ASD	09199490	40%6	319	ë
	461	09199880	40:4	215	•
	488	09193020	41:8	301	ā
	463	09193820	40.0	319	•
	454	09193420	1001	315	
	458	06966170	38 6 9	331	ä
	496	09193520	4166	302	မ
	417	09194020	4173	305	e i
	450	09194860	4161	\$67	ai .
	459	CP 194428	40-8	311	ı.
	450	09194680	46.3	863	
	46	0719432 0	37.6	346	::
	462	09198020	43.1	289	
	443	09195220	•••		3
•	464	09198420	47.4	258	01
	465	09198820	40÷0	310	:
	244	09195880	40.1	318	
	467	04808080	43.0	890	ė
·	468	09200220	40.5	314	ä
	449	09900480	41.6	308	ä
	670	09800880	~·· ~	7.7.7	2
	471	09600360	48:1	198	
	679	0401080	40.9	310	•
	473	09801880	3974	391	
	474	00201420	44.3	279	•
	475	66801680	40.4	315	•
	476	69201820	40.1	315	•
	677	09020200	84.5	899	•
	478	64505950	40.0	310	•
	496		44.0	83 i	÷
	360	64865630	40.0	315	•
	45.	0#808380	4.30	2 9 0	¥
	488	0208026	3970	369	•
	499	6456462 6	40.6	212	•
	484	6469420	43-1	289	
		04293429		•	8
	635	05 66.35 3 0			8
	457	_ u	4145	\$ 63	
	466	C38ACBEO	37.6	340	=
	ASS	05603420	40,4	215	
	490	64804480	40.4	316	•
	€31	04404320	33.8	334	¥
	4 P S	09263920	39°8	321	
	499	0344084C	49.1	315	₩.
	496	CP 6 C 5 e 8 C	59.3	224	è
	498_	_Wights	4909	299	
	496	09603880	47.4	£\$5	•
nga amina.	669	68810850	49.4	260	-
	476	65610500	44.1	eto	•

499	09810480		303	•
£00	09210420		319	`
801	098 10826		816	ف
809	09211636		307	•
903	09811880		87.6	æ.
\$04	09911480		301	•
50 5	09×11620	• ••		1
506	09911890	48.1	898	
763	09818020		289	<u>.</u>
506	69212220		585	- -
509	09212420	41.9	301	-
610	09819680	43.4	286	•
511	0818680	38:3	338	•
518	09813020	40.5	314	· - · · -
513	09213220	41.5	301	- -
514	09813420	41.5	303	•
815	09213420	48.1	898	•
514	09813880	37.0	384	- 5
517	09814080	41.1	307	ė
516	09914990	41.5	303	
519	09214420	39.9	320	•
580	09914680	45.8	267	
981	09814590	1.5	303	-
529	09215020	40.6	314	<u>.</u>
593	09815280	42.1	296	
584	09215420	41.5	303	
595	09215420	43.1	689	•
526	09215820	43.1	689	_
527	03886050	41.5	303	•
526	09220226	4176	302	•
589	09890490	43.3	888	•
539	09880480	40.4	315	
531	098 50 880	42.9	890	•
532	09221020	41.9	301	÷
533	09221220	38.9	331	
534	09221420	44.3	840	•
635	09221620	41.9	301	•
536	03551550	41.6	302	•
657	035\$\$6050	43.4	286	•
538	04464660	43.6	294	•
559	09282420	42.5	294	•
540	03585950	42.0	899	€
541	06535350	47.4	255	•
542	08883020	43.6	285	•
649	04883880	•••	•	2
660	09923420	41.9	301	•
545	09225420	37.1	359	•
843	09983880	43.0	890	
54 7	CPERACED	48.9	890	.
548	05854880	49.6	204	· •
649	0026420	47.6	263	•
350	03884620	41.5	303	•

		44549NO	43.5	. 89 5	•
		788886	3961	389	-
		4825 8 20	43:3	205	₽
_	-	7825420	42:0	899	-
		488660	4871	668	—
		9825880	40:4	316	•
		723 0020	49:6	253	•
		9 830229	4276	89 8	<u>~</u>
		9830 400	48.6	9 92	÷
		98 3048 0	40.6	318	š
		353688 0	40.8	311	•
		9831660	48.0	301	-
		- 0751684	4370	29 0	ä
		9831580	4879	299	©
	*	9831420	4376	890	•
		9231620	42.4	295	•
		9832020	4116	308	ei.
		9232320	42,5	298	•
		9238460	42.5	294	÷
		9838480	35.1	339	
		9 838 580	4179	301	•
	-	9233626	46-8	259	æ
	r	9933880	41:B	303	÷
		9233420	4378	235	÷
		9233620	46.0	865	•
	-	8833880	4175	303	$\stackrel{\sim}{\bullet}$
		9234020	43.6	264	•
		0934890	43.0	690	€
		9834420	4170	309	•
		9234620	4375	265	•
		9234890	42.4	2 95	**
			41.4	305	•
_	-	P235220	43.5	285	~
-		P235420	39:0	320	•
			40.9	310	Ø
				895	•
			40.4	315	-
			44.1	979	•
				294	.
			41.3	306	÷
59			40%	311	=
98			42.8	202	•
B				301	-
. 65			48.0	580	•
61				315	•
5%			38.6	334	4
55				259	♣.
5%		_		306	•
89				307	9
60				284 	•
66				384 262	•
60	HE 16	1003080	45.5	26 3	Ġ

693	10603820	39.1	389	•
 664	10003490	44.3	819	¥
605	16003480	41.0	309	ė
606	10003820	4176	302	•
607	10004620	42.8	292	•
608	10004220	41.5	301	ë
609	10004480	48.1	896	¥
 410	10004620	4674	262	•
611	10004620	40.6	312	•
619	10005020	4178	301	#
613	10005220	49.6	318	4
614	10005480	4474	278	÷
615	10005680	4174	305	<u>.</u>
 616	10003820	41.4	308	,
617	16010020	48.5	894	
616	10010220		·	X
619	10010420	41.3	306	ê
¥ 1				

EXPLANATION OF COMMENT CODES

- DUD SCHEDULED DETONATION TIME IS LISTED
- SUS DETG. TYOM AT VEDNS DEPTR DETONATION SICHAL NOT RECORDED
- DETONATION SIGNAL NOT PROCESSABLE

TABLE 6

SUS SHOT STATISTICS FOR SQUARE DEAL

 FOR USUS	Kiresport	DURING AUGUST, 1973		
340 *	Apprixinate Detonation	BUBBLE PULSE PERIOD	Calgulated Shot depth	Coment Code
 , , , , , , , , , , , , , , , , , , ,	(ULUS) BRIT	(85 2C)	(FT)	•
 ĺ	14915020	39.9	320	•
 🙎	16015220	39-3	327	~
3	16015429	41.5	393	₩
	16015620	41-4	305	
5	16015820	41.0	309	~
 6	18080030	44.6	27 5	
7	16020220	41:0	30 9	~
 8	16020420	42.5	294	· 🕳
9	16020620	40.9	310	<u>.</u>
 10	16020820	40.6	312	6
 11	16021020	44.6	276	
 12	16021880	40-5	314	*
83	16021420	43.0	290	=
 14	16021620	41.3	306	•
 15_	16021820	41.9	301	—
16	16022020	43.6	284	#
 17	16022220			
18	16022420	37 • 3	350	. 🐞
 19_	15022620	42.3	297	
20	16022820	41.4	305	*
 21	16023020	37 31	358	
88	16023220	39:3	587	=
23	16023420	45.1	27 1	·
24	16023620	41.3	306	a
 85	16023820	45.8	259	¥
26	16024020	39.8	381	÷
 27	16084820	43~8	283	÷
28	16084480	43.9	282	:
 89	16024620	4378	283	<u></u>
30	16024820	42.1	296	÷
31	16025020	46.6	260	•
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33	16085420	40.1	318	. .
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 25	16025520	42.0		
 34	16030080	40.4	315	•
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	48	16031080 16031080	43.0 41.4	890 308	
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	63	1503 [480	42.0	299	<u>.</u>
	44	16031620		306	¥
	45	16031820	41:3 40:9	310	<u>.</u>
	66	16032020		309	=
	47	19035784	41.0	309	-
	48	14032420	AC 2	08.0	8
· -	49	16032620	45.3	270	•
	80	16032620	44.6	276	
_	53	16035020	40%4 41%9	315 301	
	58	15033980	42.3	297	- 36
	53	16033480		894	
	54	16033620	42.5		5
	85	16033680	41.5	303	
•	56	16034020	43.0	29 6	⇔ ≥
	57	16034280	40.6	318	••····································
	58	16034420	48.0	899	•
	39	16054680	47.9	251	
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	61	16035020	40.4	315	. •
	68	16035220			3
	33	16035420	40.3	316	•
	54	16035680	40.8	311	•
	65	16035580	40:1	318	
	66	16040020	48.4	295	=
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	68	16040420	40.8	311	~
	69	16040620	41:4	305	=
	70	16940820	40:9	310	¥
	71	16041020	46.1	264	.
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	74	16041620	44.8	275	•
	78	16041820			
	76	16049020	41.5	303	•
		16042820	46.9	<u> </u>	_ _
	76	16042420	3975	324	ö
	79_	16042620	39:3	327	ĕ
	80	16042820	4170	309	¥
	51	16043095	39%8	321	•
	88	16043220	39.9	380	•
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	85	16043880	40:8	311	.
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	05	16051620	41.8	303	=
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		16054820	41:4		
		14055020	4153		
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		6055820	40.3		
		16060020	4104		
		6060220	4178	301	-
		6060420	4159		.
		6060620	41.0	309	
		6060080	41:4		<u>.</u> -
		6061020	41.6	308	
		6061220	45.8		<u>-</u>
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		6061620	41.3	864	e
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	147	16064220	••	7 7.X	
	148	16064420	41.3	306	ï
	149	16064680	38-0	341	₩
	150	16064820	36.3	336	:
	151	16065020	41%	301	<u>.</u>
, ·	168	16065220	41.4	305	÷
	153	16065480	40-9	310	ø.
	184	16065620	39:1	389	~
	155	16065820	38~3	338	=
	156	16070080	4000	319	=
	157	16070220	43.1	289	-
	155	16070420	41.9	301	~
	159	16070620	40.3	316	
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	161	16071020			3
	162	16071220			3
	163	16071420			3
	164	16071620	40.9	310	•
	165	16071820	4171	307	-
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	168	16072420	42.4	295	=
	169	16072620	43.6	264	-
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	178	16073020	40.0	319	•
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	154	16078620	43-1	259	e i
	185	16075820	44.4	278	•
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	187	16080820	39.9	380	~
	186	16080420	42.0	899	
	159	14080620	42:1	898	=
	190	16080820	41.3	308	<u></u>
	191	16081020	44.8	259	•
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	193	16081420	40.1	310	
	164	16091690	rent of the contract	, -	
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	197	16062220	47 -8	252	•
	198	16088420	48.3	899	
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	201	16083020	38.9	331	 •
	808	16063980	40:3	316	•
	203	14053420	4156	308	
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	205	16063620	37:1	352	ë
	206	18054020	41:6	308	¥
	207	16054220	43:1	269	ä
	504	16053420	48:1	293	ë
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	811	16055920	42:9	042	
	816	16088880		77	Į
•	213	16865420	42.9	290	Ĭ
	234	16063620	42.4	295	ä
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	819	16090620	4101	307	•
	220	16090620	4001	318	•
	221	16091080	40.9	310	
	222	16091220	44.1	279	
	223	16091420	41.0	309	en
	824	16091620	43.1	869	•
	225	16091820	40%	311	÷
	226	16092020	4000	319	¥
	227	16092220	39.3	387	<u>.</u>
	828	16092420			<u>8</u>
	859	16098620	41.1	307	-
·	230	14092820	40.9	310	<u>.</u>
·	231	16093020	4171	307	
	232	14093880	43.8	253	
17	833	16093420	48.3	297	ani.
'* 	834	16093620	39.5	324	
11	235	16095880	40°6	311	
	236	16094020	42.1	898	
ış	837	16094020	48.4	1	.
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9	839	16094620	40%4	915	
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8	241	14496020	4066	312	-
	848	14095220	40.0	319	<u>.</u>
,	243	16095480	43-1	289	•
	244	16093620	43.0	200	•
¢	245	16098820	48.5	894	•
	846	16100080	43.9	252	
5	847	14100220	47.5	254	•
	846	16100480	46-6	260	•
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	249	16100620	42.1	298	•
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	231	16101020	42:0	299	-
	254	16101220	41.8	301	
	253	16101320	48.4	295	<u> </u>
	254	16101680	43.5	255	
	255	16101880	40:1	318	
	200	16108080	48:0	299	· <u>-</u>
	257	16162220	48.6	293	=
	258	16102480	40.5	314	•
	259	16102620	39:9	320	
	860	15102620	47:9	25)	=
	261	16103680	41:8		· ·
	868	16103220	3,49	<u> </u>	. =
	263	16103480	41.0	30 9	3
	264	16103620	37:9		
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	246	16104020	4170	309	₫
	247		40.8	311	•
		15104220	41;4	305	<u>.</u>
	265	15104420	48:3	297	
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	870	16104820	40.8	311	•
	271	16105020	4370	890	•
	278	16105220	44.0	261	.
	273	16103480	41.5	303	
	274	16105620	39:5	324	ù
	275	16105820	36.5	336	ä
	274	16110080	39.4	386	•
	877	16110220	40.9	310	a
	276	16110420	37:6	346	ä
	279	16119620	47.6	853	
	058	16110820	4376	264	•
	281	16111020	42:5	294	•
	282	16111220	43.5	285	=
	283	16111420	43:4	256	*
	254	16111620	41.8	301	\(\delta\)
	288	16111680	41.9	301	
	286	16112020	4279	840	
	287	19119220	4163	306	•
	582	16112820	39:3	327	•
n=	289_	16112620	49.8	898	=
	290	16112820	40:4	518	**
	201	16113020	47:0	231	
	200	16113220	4378	289	•
	29 3	16113420	48.0	899	•
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	363	16118420	40:3	593	4
	304	16115620	46:8	356	¥
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	364	16120020	44.0	294	•
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	307	16130420	42.5	294	
	308		39:4	384	•
	309	16120680	43.8	253	•
	310	16120820	4173	306	=
	311	16121020	4361	8L P	•
	318	16181880	40:5	3 € 44	ä
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	316	16122020	47.9	251	•
	317	16186860	4179	301	•
	316	16122420	37:4	255	¥
	319	16122620	€0:6	312	ä
	320	16165880	4168	301	<u>`</u> .
	321	16123020	42.4	29 S	÷
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•	394	16183680	46.1	318	<u></u>
	325	16123820	4558	301	á
	326	16194090	42.5	265	
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	339	16124620	42.3	297	:
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	333	36125420	48.8	8 9 8	~ ~
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	338	16130020	42.6	898	
	337	16130420	41.8	301	_
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	340	16136886	3975	324	•
	241	16131080	39: 6	383	
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	367	1613260	40 .6	318	•
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	346	16132620	37.8	345	. •
	380	16132820	41.6	302	•
	381	16133090	4918	283	•
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	363	16133489	41.3	306	45
	354	16133680	42.1	898	÷
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	356	16134080	40%	315	ä
	387	15134920	4114	305	d
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	361	16135020	* - 4 # *	• •	3
	368	16135920			3 3 -
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	365_	16135820	· • •		1
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	368	16140480	42:5	292	=
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	373	16141420	40.9	310	•
	374	16141680	3978	321	-
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	376	16142020	40.6	312	4
	577	16142220	4176	308	=
	378	16142420	40.9	310	
	379	16142620	44.8	275	÷
	380	16146880	4676	260	•
	351	16143020	3874	337	÷
	388	16143220	46:4	868	٠
	383	16143420	42.0	290	49
	384	16143620	42%	293	
	365	16143520	4875	\$94	¥
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	391	16145020	40.6	311	•
	398	16145880	4178	307	•
	393	16145428	49.9	890	~
	394	16148620	40.6	318	4
	398	16145980	40.5	311	_ _
	396	16150020	42.1	208	4
	307	16150920	43.0	296	•
	396	15150420	4170	301	=
	399	16130420	42.1	888	•
	460	16180820	4653	863	~
 	401	18181080	47:4	255	
	409	16151620	43.1	289	٠
	603	16151480	48.3	897	-
	404	16151680	41.8	306	•
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	408	16151820	40,9	310	
	406	16152080	40.8	311	•
	407	18152820	37:3	350	
	408	16139420	42:0	299	:
	409	16152620	42:5	294	•
	410	16152620	3979	320	ä
	411	16153020	41.5	301	•
	418	16153220	38.6	334	ä
	413	16153420	49:3	297	ä
	4l4	16153620	40.8	311	¥
	416	16153820	40:8	311	•
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•	417	16154220	44.4	276	é
	318	16154420	48.3	297	•
	419	16154620	39.3	387	•
	480	16154820	40.4	315	•
	481	16158020	3974	326	<u>.</u>
	428	16155220	4370	890	ä
	423	16155420	42:9	290	ä
	424	16155620	4666	240	
	425	16155820	41.4	305	æ.
	426	16160020	39:9	320	- :
	427	16160220	39.0	32 9	
	428	16160420	40.5	314	÷
	489	16160620	37:1	362	•
	430	16150820	38.0	341	· •
	431	16161020	41:1	307	· -
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	435	16161820	43.0	290	
	436	16162020	41.9	301	•
	438	16162880	46.6	260	.
	439	18162420	42.8	305	
	440	16162620	42.5	294	vi
	441	16162880	**		Ĭ
	442	16143020	48,9	963	
	443	16163120	40.6	318	-

EXPLANATION OF COMMENT CODES

- ## DUD SCHEDULED DETONATION TIME IS LISTED
 ## SUS DETONATION AT VIDES DEPTH
 ### DETONATION SIGNAL NOT RECORDED
 ### DETONATION SIGNAL NOT PROCESSABLE

References

- "SUS Quality Assessment", December 1, 1973, Contract N00014-73-C-0484, Underwater Systems, Inc., Unclassified.
- D. E. Weston, "Underwater Explosions as Acoustic Sources", Proc. of the Physical Society, Vol. LXXVI, p. 233, 1960.



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Ref:

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- 2. The LRAPP documents listed in enclosure (1) have been downgraded to UNCLASSIFIED and have been approved for public release. These documents should be remarked as follows:

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Report Number	Personal Author	Title	Publication Source (Originator)	Pub. Date	Current Availability	Class.
55	Weinstein, M. S., et al.	SUS QUALITY ASSESSMENT, SQUARE DEAL	Undersea Systems, Inc.	750207	ADA007559; ND	n
BKD2380	Unavailable	WESTLANT 74 PHASE 1 DATA SUMMARY (U)	B-K Dyanmics, Inc.	750301	NS; ND	n
TM-SA23-C44-75	Wilcox, J. D.	MOTION MODEL VALIDATION FROM LRAPP ATLANTIC TEST BED DATA	Naval Underwater Systems Center	750317	ND	n
RAFF7412; 74-482	Scheu, J. E.	SQUARE DEAL SHIPPING DENSITIES (U)	Raff Associates, Inc.	750401	ADC003198; NS; ND	U
PSI TR-004018	Barnes, A. E., et al.	ON THE ESTIMATION OF SHIPPING DENSITIES FROM OBSERVED DATA	Planning Systems Inc.	750401	AD CAR SEL	n
NUSC TD No.4937	LaPlante, R. F., et al.	OUSTIC BUOY SYSTEM (MABS)	Naval Underwater Systems Center	750404	ADB003783; ND	n
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